

IPO Gaslift Design Using Valve Performance

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Abstract

- Gaslift design has been practiced successfully using the Thornhill/Craver equation to size ports but the gas flow predictions could be 3-4 times the actual flow rate for 1" IPO unloading valves.
- The use of Thornhill/Craver as the means for sizing ports is no longer necessary.
- Tested valve performance correlations are available that are within +/-15% of actual flow rates for all commonly used valves.

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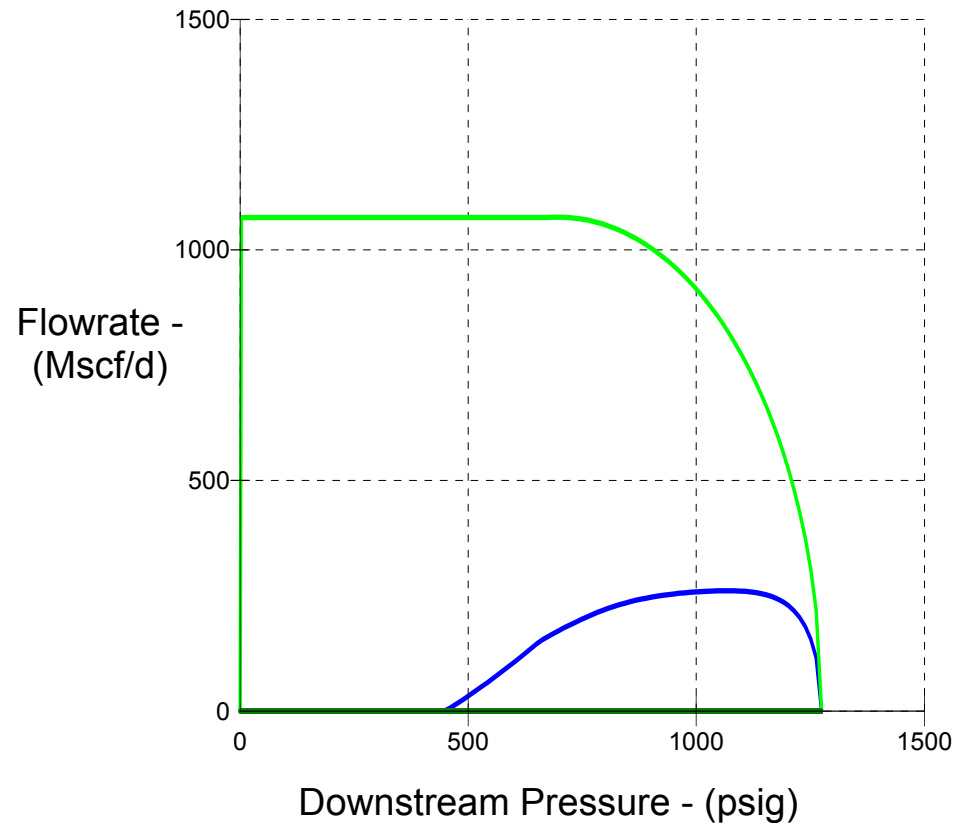
Thornhill Craver

- Use of TC to calculate flow passage through gaslift valves assumes the port is full open and the flow path is unobstructed but...
 - Loadrates of IPO valves do NOT allow the valve to fully open when annulus pressure (P_{iod}) reaches opening pressure (P_{voT}).
 - IPO valves usually have downstream obstructions including the backcheck which further restricts flow passage.
- TC is OK for orifice valve gas passage calculations.
- Flow passage through 1-1/2" IPO valves is much better than for 1" IPO valves.

1" IPO Valve Performance

- TC will predict rates that are 3-4 times the actual flow rate
- T/C predicts orifice flow but valves throttle closed!
- TC was handy when nothing else existed but now something better does exist.

T/C versus Tested for 1" IPO with 12/64ths port

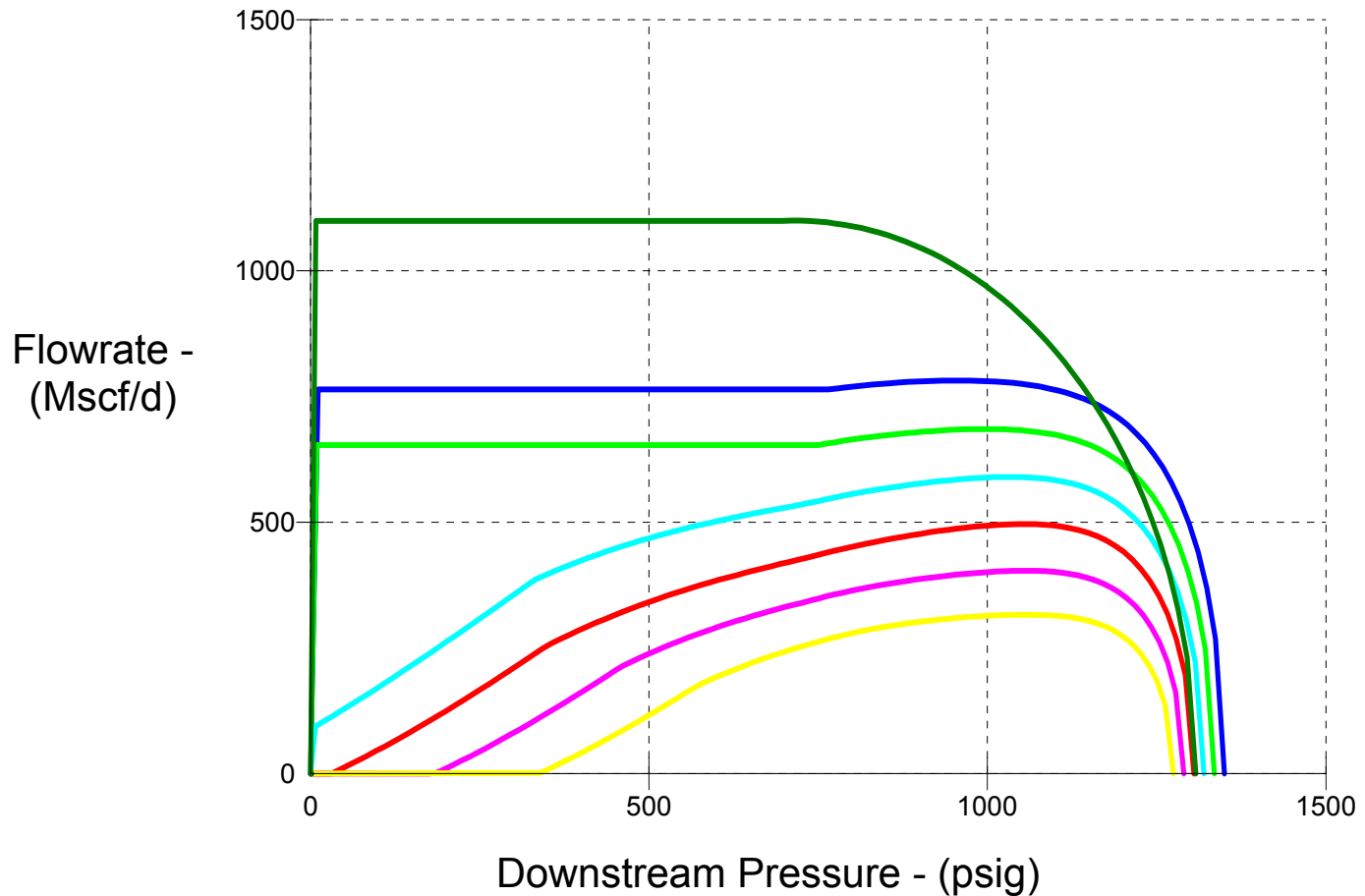


Typical Performance of 1" IPO Valves

- When the annulus pressure (P_{iod}) is equal to the opening pressure of the valve (P_{voT}), the valve will throttle to the closed position when tubing pressure goes to atmospheric.
- P_{iod} about 20-30 psig **ABOVE** P_{voT} is required to achieve orifice flow.
- Current gaslift designs will yield P_{iod} about 20-30 psig **BELOW** P_{voT} . Net gap - about 40-60 psig.

Typical 1" IPO Flow Rate

1" IPO w/ 12/64ths Pvcot 1308 Temp 130



Flow Rate Comparison

- At $P_{iod} = P_{vot}$ and $P_{tf} = \text{Transfer...}$
 - Thornhill/Craver predicts about 1.1 MMscfd
 - Actual valve performance is about 300 Mscfd at maximum flow and...
 - The valve throttles closed at $P_{tf} = \text{Transfer}$
- About 1/4th the gas passage at maximum flow and NO injection at the transfer pressure.

But the IPO Design Technique Works !!

- The current IPO design technique as practiced using the API RP 11V6 has been successful!
- TC flow rate prediction is far in excess of the actual amount the valve can pass but it seems to work !!
- There are several reasons...
 - Surface gas injection rate versus valve gas passage
 - Actual annulus pressure at the valve versus design pressure
 - Multiple unloading valves open rather than single point
 - Help from the reservoir

Injection Rates

- **Boyles Law!**
 - In a fixed volume (annulus) if more gas is injected at the surface than is flowing out through the valves, the pressure will rise.
 - When the first unloading valve uncovers, the surface gas injection rate is adjusted to the expected injection rate.
 - This rate is usually far in excess of the amount that can pass through the unloading valves consequently, the surface injection pressure will continue to rise.

Annulus Pressure

- The annulus pressure (P_{inj}) will be at kick-off pressure when the first valve uncovers.
- It is expected the annulus pressure (P_{inj}) will drop when the second valve uncovers but...
 - If the flow rate through the valves is less than is being injected at the surface, this will not happen!
 - The wellhead injection pressure will remain near kick-off pressure and the surface injection rate will drop to match the flow rate through the valves.
- The anticipated injection pressure drop did not happen!

Lower Valves Uncover

- The top valve remains open when the second valve uncovers and begins injection. This is expected.
- If the combined gas flow rate through both unloading gaslift valves is less than the amount injected at the surface...
 - The annulus pressure will not drop!
- Unloading valves will remain open until the total flow rate through all open unloading valves exceeds the amount injected at the surface.

Multipoint Injection

- Is this a problem?
 - NO! During unloading multipoint injection is not a problem.
 - YES! If the operator was recording the annulus pressure during unloading and expected to see a pressure drop as each lower valve uncovered, he will not see it. He does not know where injection is taking place!
- Is the designed annulus pressure drop of 20 psig at each valve necessary?
 - YES! The objective is to ensure that the valves close in sequence from the top to the bottom. Designed pressure drops at each valve will ensure this occurs.

Solution Gas Helps

- It is very possible that 3-4 unloading valves will be open and injecting gas before the operating valve is reached.
- As gas injection works deeper, eventually the reservoir will begin inflow.
- Help has arrived! If the GOR is reasonable then the lack of gas injection rate from the valves will be made up by the reservoir.

The API Design Works but...

- The API design technique does work but not the way it was expected to work.
 - Pressure drops may not occur as each valve uncovers
 - Multiple unloading valves will be open
 - Solution gas may be required to assist with unloading
- If the well has a higher PI than anticipated or the water cut is higher, it may not be possible to reach the operating valve.
- This is a little risky. Can we do better?

Can We Design Better!?

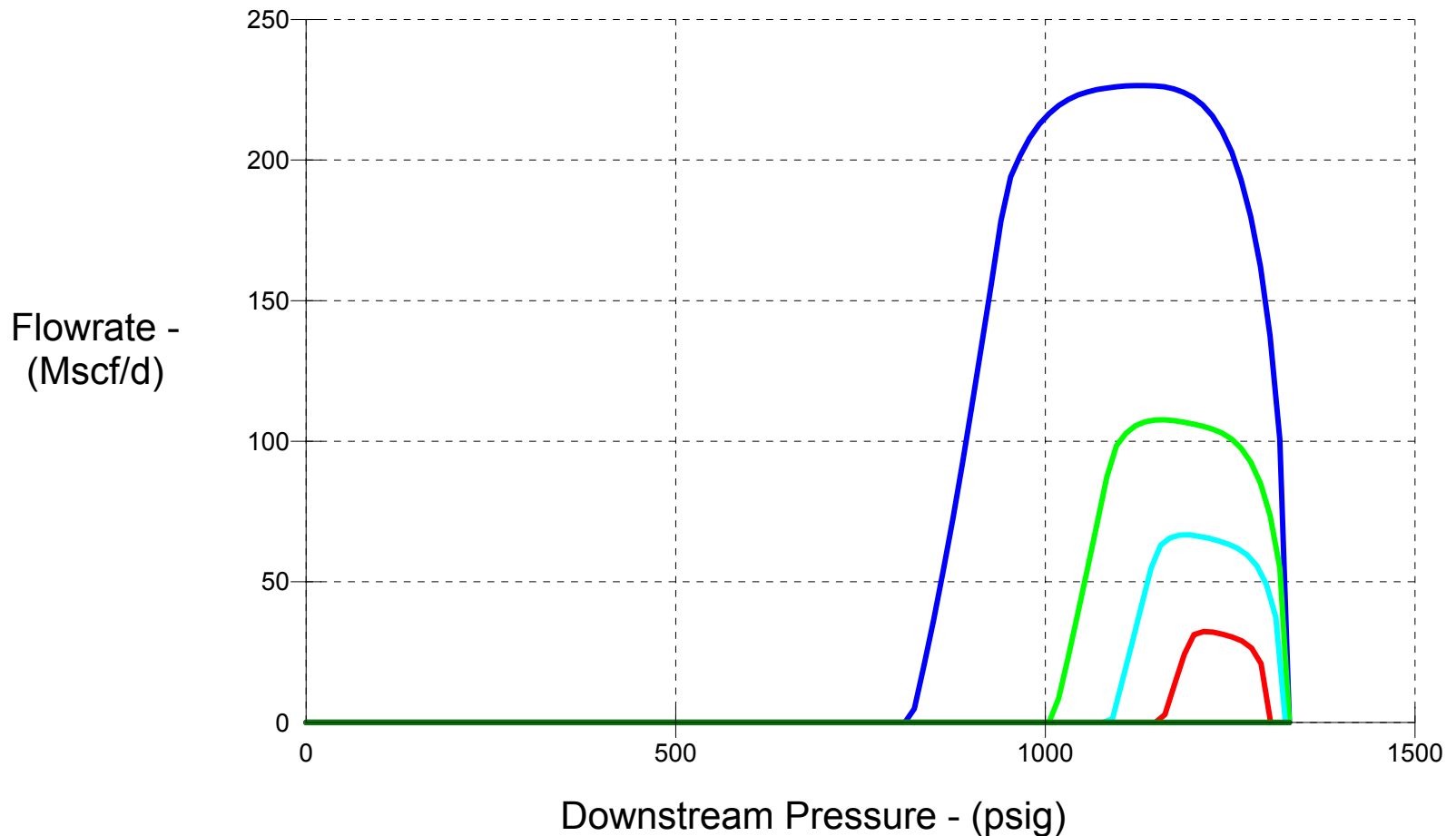
- Understanding the actual flow performance of 1" IPO valves gives us several choices...
 - Use larger ports
 - Take larger pressure drops between valves
 - Arbitrarily lower the set pressure of the valves
 - Reduce the kick-off pressure used for design
- Lots of options. What do we do?

Using Larger Ports

- For the remaining four valves in the example, at the designed annulus pressure, the valves with 16/64ths ports still do not pass as much gas as is being injected at the surface.
 - Consequently, the annulus pressure will be higher than anticipated. This is good!
 - There will be a slight annulus pressure drop as each valve begins injection but not as much as expected.
 - If the operator is recording P_{inj} and Q_{inj} during unloading, the analysis could be confusing.

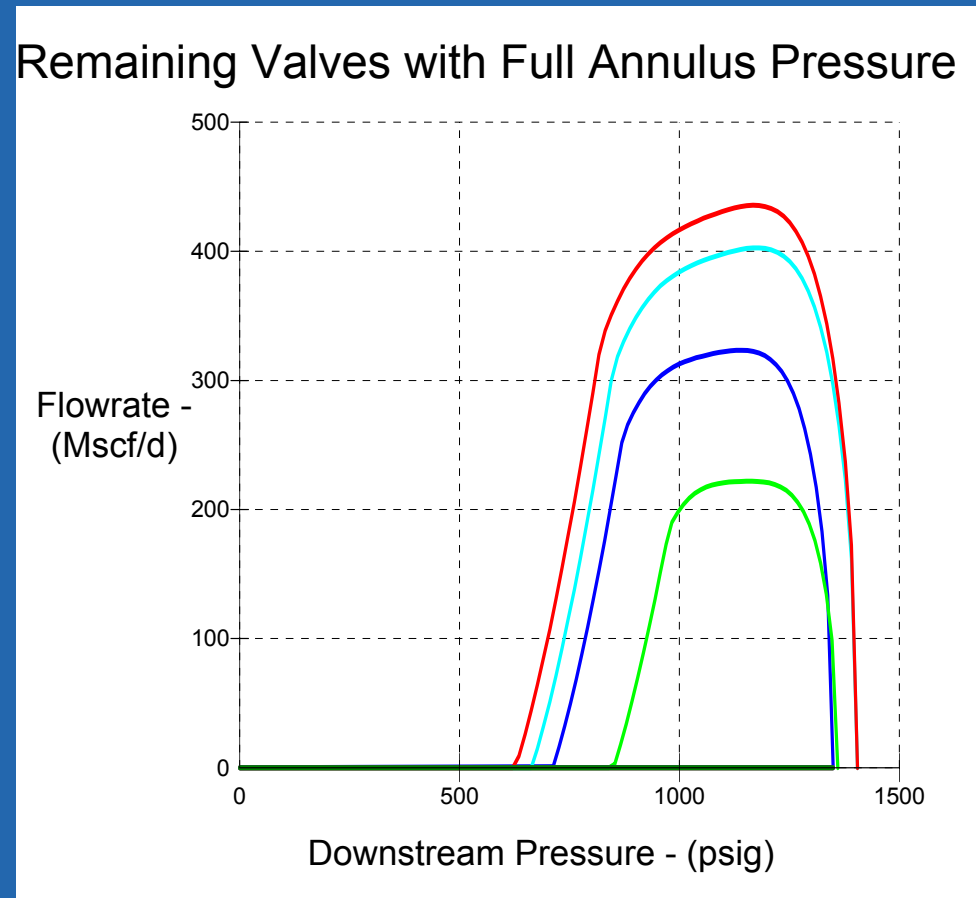
16/64ths Ports - Design Annulus Pressure

Remaining Valves with 16/64ths Ports



16/64ths Ports - Full Annulus Pressure

- If annulus pressure drops did not occur, then each lower valve has 20 psig additional annulus pressure.
- Flow rates through the valves are significantly higher!
- More pressure, more valve opening, and more flow rate!



Full Annulus Pressure

- With 16/64ths ports, the combined valve flow rates at full annulus pressure will be greater than the amount injected at the surface therefore...
 - The annulus pressure will drop as each lower valve uncovers but probably not the full 20 psig per valve
 - Multiple valves will be open
 - Valves will close and re-open many times
 - Unloading will experience many slugs
- Larger ports at the lower unloading valves is a definite possibility.

Larger Pressure Drops at the Valves

- Larger pressure drops (30-50 psig) at each valve will...
 - Increase the flow rate through the lower valves
 - Provide more positive indication on injection depth
 - Provide better protection against multipointing
- Larger pressure drops might work but...
 - The valve spacing will be closer
 - It may not be possible to reach the objective injection depth
 - If multipointing does occur, larger slugs
- This is a possibility if the objective injection point is shallow but for deep injection points and high PI wells this will not solve the

Lower the Valve Set Pressures

- If the spacing is left the same and the set pressures of the valves are arbitrarily lowered by 20 psig...
 - valves will flow more gas
 - It will be more difficult to close the valves when the orifice is reached
 - As the water cut rises, upper valves will open more easily
- Arbitrarily lowering the set pressures will invite multipointing and slugging at a later date.
- Not a good option as a long term solution

Lower the Design Pressure

- Decreasing the design pressure 50 psig from the available pressure has many benefits
 - Valves will have an additional 50 psig above opening pressure
 - Valves will have flow performance much closer to orifice flow
 - There is a good chance single point sequential injection will occur during unloading.
 - The annulus pressure will drop as each valve uncovers.
- The disadvantage is that the objective injection point will be shallower by several hundred feet.

Your Choice!

- Larger ports work for the lower valves
- Larger pressure drops at each valve significantly reduces the objective injection depth
- Lowering the set pressure could invite multipointing at a later date when water cut rises
- Lowering the kick-off pressure 50 psig below the available pressure reduces the depth of injection but is safe.

Knowledge and Experience

- The modifications suggested have been well known but experience with “**the art**” of gaslift was required to know which ones to use. Valve performance models add **science** to the decision making.
- Gaslift is forgiving and flexible. Anybody can produce a gaslift design without the use of valve performance models and it will probably work but...
 - **Using valve performance models is a definite benefit!**

Conclusions

- The existing API spacing technique works but will be much safer when the kick-off pressure is 50 psig less than the pressure available.
- Larger ports may be required at the lower valves.
- Increasing pressure drops between valves helps but reduces objective injection depth
- Arbitrarily lowering set pressures invites problems
- Having a valve performance model to help

Thank You!

- Using good valve performance models is possible today!
 - Several gaslift design programs now offer the ability to use valve performance models during the design stage.
 - WinGlue
 - SNAP
 - Prosper
 - and there may be others
- Thank you for your attention and patience!
- Please contact SPE for a copy of the paper -
SPE 109694